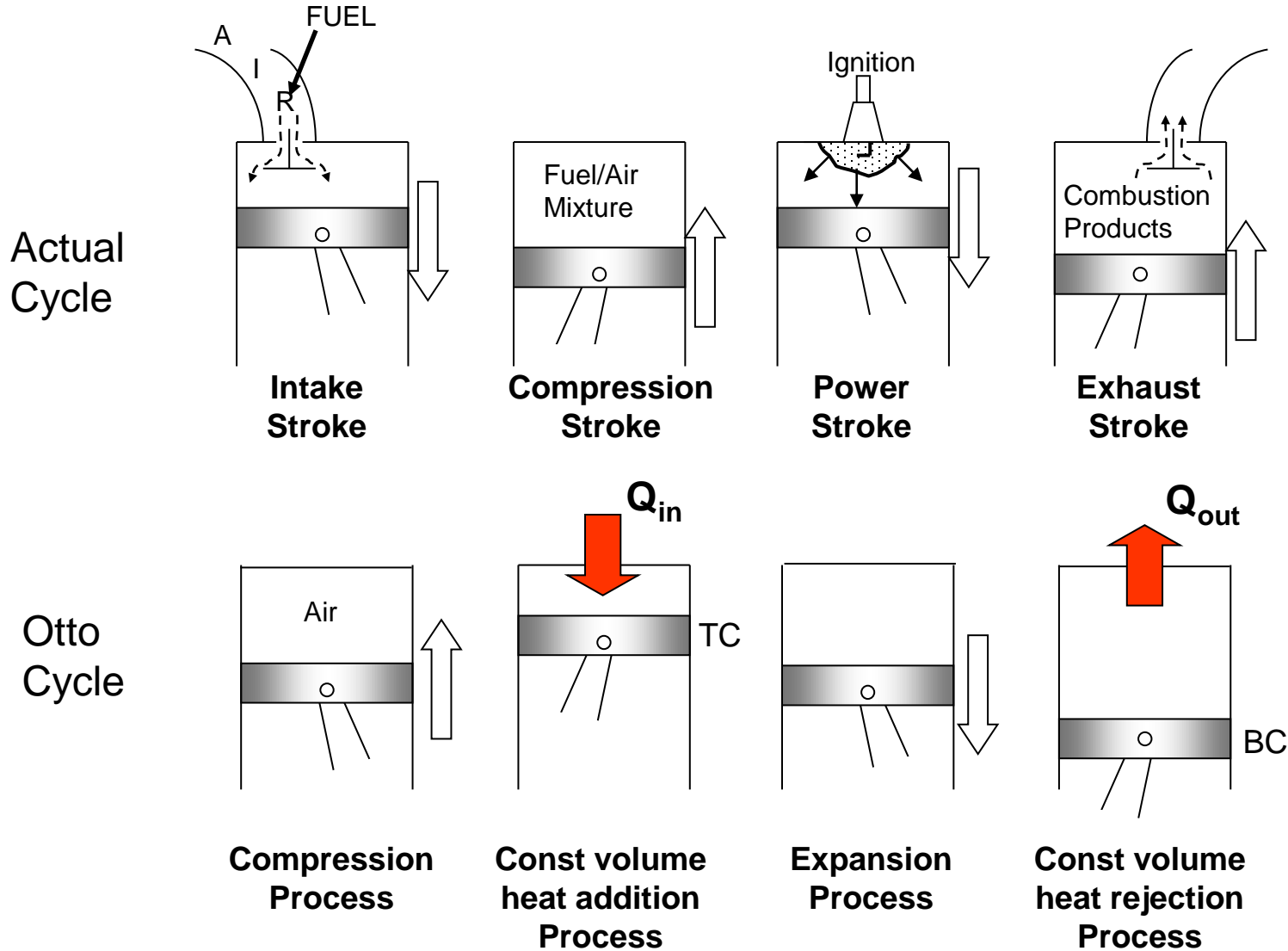


Thermodynamic Cycles

Air-standard analysis is a simplification of the real cycle that includes the following assumptions:

- 1) Working fluid consists of fixed amount of air (ideal gas)
- 2) Combustion process represented by heat transfer into and out of the cylinder from an external source
- 3) Differences between intake and exhaust processes not considered (i.e. no pumping work)
- 4) Engine friction and heat losses not considered

SI Engine Cycle vs Air Standard Otto Cycle



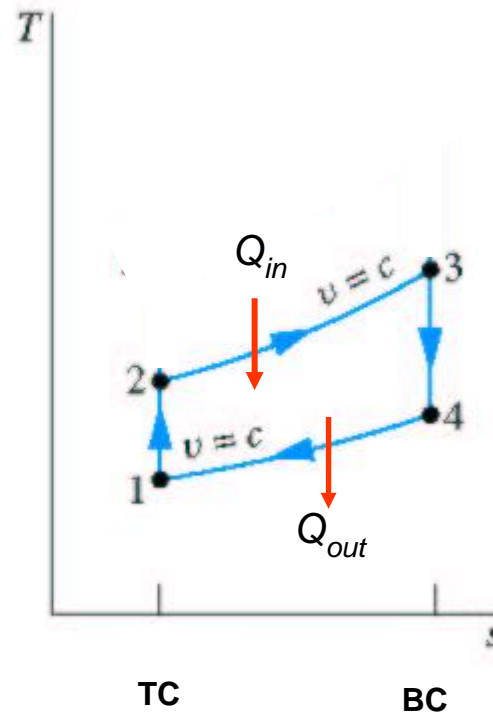
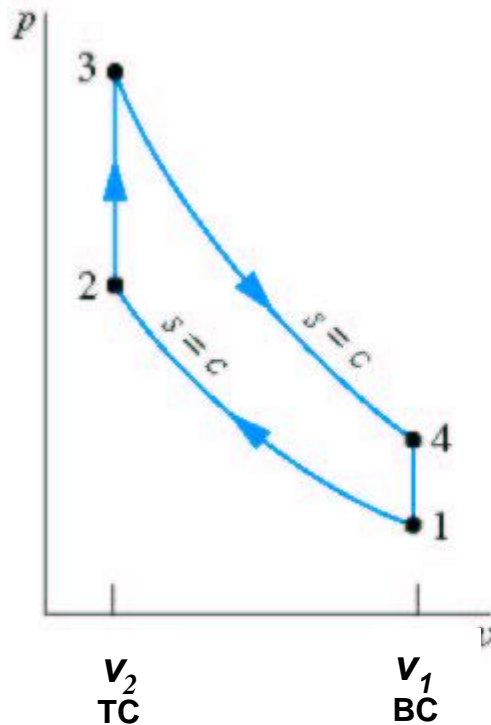
Air-Standard Otto cycle

Process 1 → 2 Isentropic compression

Process 2 → 3 Constant volume heat addition

Process 3 → 4 Isentropic expansion

Process 4 → 1 Constant volume heat rejection



Compression ratio:

$$r = \frac{v_1}{v_2} = \frac{v_4}{v_3}$$

First Law Analysis of Otto Cycle

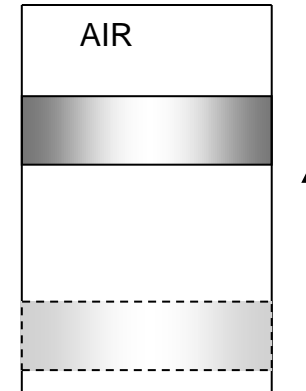
1 → 2 Isentropic Compression

$$(u_2 - u_1) = \cancel{Q} - \left(-\frac{W_{in}}{m}\right)$$

$$\frac{W_{in}}{m} = (u_2 - u_1)$$

$$\frac{v_{r_2}}{v_{r_1}} = \frac{v_2}{v_1} = \frac{1}{r}$$

$$R = \frac{P_2 v_2}{T_2} = \frac{P_1 v_1}{T_1} \rightarrow \frac{P_2}{P_1} = \frac{T_2}{T_1} \cdot \frac{v_1}{v_2}$$



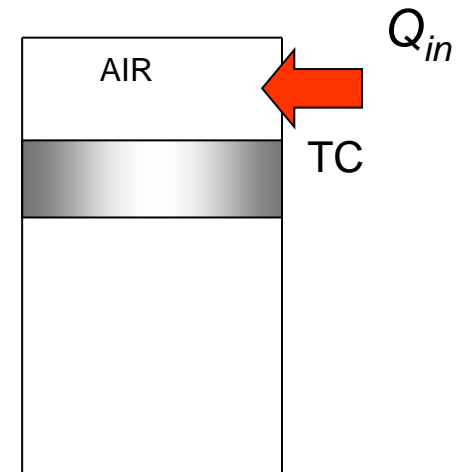
First Law Analysis of Otto Cycle

2→3 Constant Volume Heat Addition

$$(u_3 - u_2) = \left(+\frac{Q_{in}}{m}\right) - \frac{\cancel{W}}{m}$$

$$\frac{Q_{in}}{m} = (u_3 - u_2)$$

$$v = \frac{P_2}{RT_2} = \frac{P_3}{RT_3} \rightarrow \frac{P_3}{P_2} = \frac{T_3}{T_2}$$



First Law Analysis of Otto Cycle

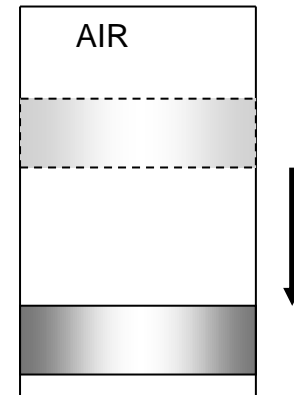
3 → 4 Isentropic Expansion

$$(u_4 - u_3) = \cancel{\frac{Q}{m}} - \left(+ \frac{W_{out}}{m} \right)$$

$$\frac{W_{out}}{m} = (u_3 - u_4)$$

$$\frac{v_{r_4}}{v_{r_3}} = \frac{v_4}{v_3} = r$$

$$\frac{P_4 v_4}{T_4} = \frac{P_3 v_3}{T_3} \rightarrow \frac{P_4}{P_3} = \frac{T_4}{T_3} \cdot \frac{v_3}{v_4}$$



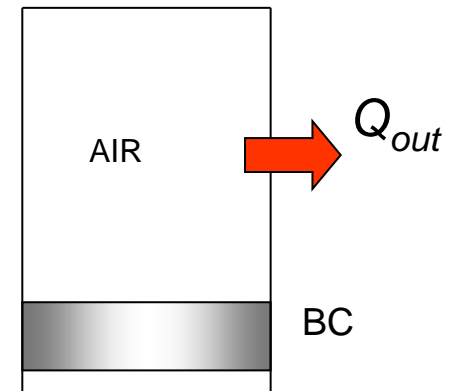
First Law Analysis of Otto Cycle

4 → 1 Constant Volume Heat Removal

$$(u_1 - u_4) = \left(-\frac{Q_{out}}{m}\right) - \frac{\cancel{W}}{m}$$

$$\frac{Q_{out}}{m} = (u_4 - u_1)$$

$$v = \frac{P_4}{RT_4} = \frac{P_1}{RT_1} \rightarrow \frac{P_4}{T_4} = \frac{P_1}{T_1}$$



First Law Analysis

Net cycle work:

$$W_{cycle} = W_{out} - W_{in} = m(u_3 - u_4) - m(u_2 - u_1)$$

Cycle thermal efficiency:

$$\eta_{th} = \frac{W_{cycle}}{Q_{in}} = \frac{W_{out} - W_{in}}{Q_{in}} = \frac{(u_3 - u_4) - (u_2 - u_1)}{(u_3 - u_2)}$$

$$\eta_{th} = \frac{(u_3 - u_2) - (u_4 - u_1)}{u_3 - u_2} = 1 - \frac{u_4 - u_1}{u_3 - u_2}$$

Cold Air-Standard Analysis

- For a cold air-standard analysis the specific heats are assumed to be constant evaluated at ambient temperature values ($k = c_p/c_v = 1.4$).
- For the two isentropic processes in the cycle, assuming ideal gas with constant specific heat using $Pv^k = \text{const.}$ $Pv = RT$ yields:

$$1 \rightarrow 2 : \quad \frac{T_2}{T_1} = \left(\frac{v_1}{v_2} \right)^{k-1} = r^{k-1} \quad \frac{T_2}{T_1} = \left(\frac{P_2}{P_1} \right)^{\frac{k-1}{k}}$$

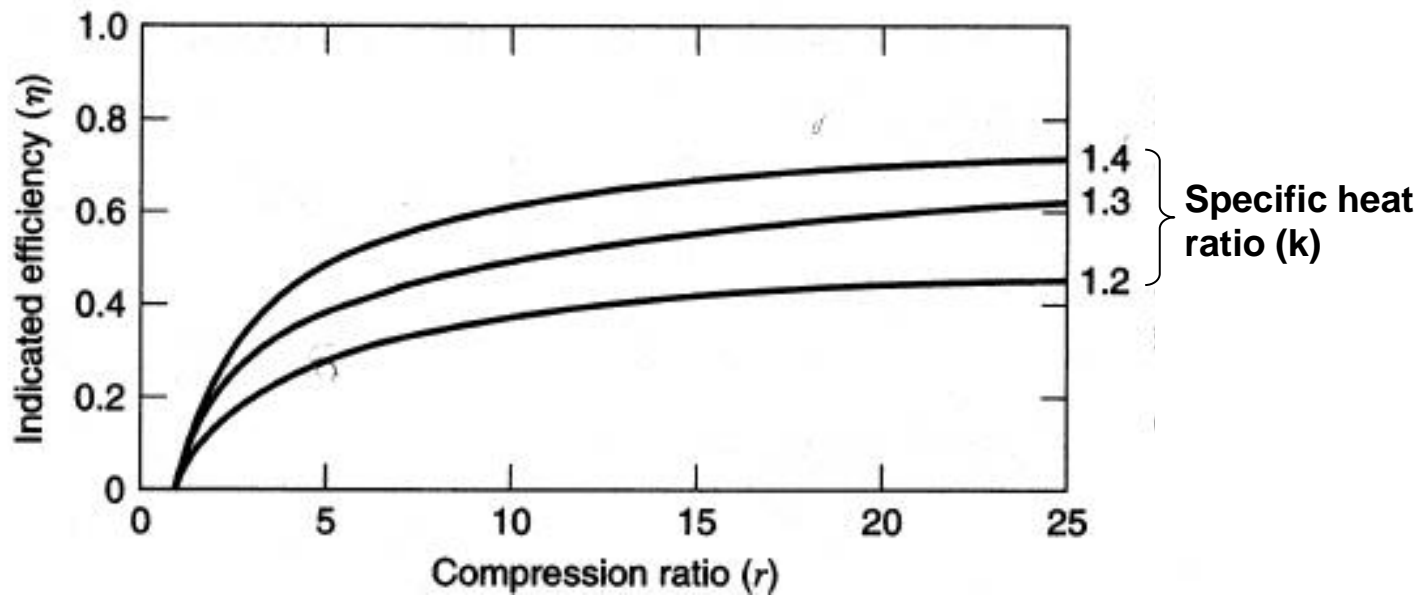
$$3 \rightarrow 4 : \quad \frac{T_4}{T_3} = \left(\frac{v_3}{v_4} \right)^{k-1} = \left(\frac{1}{r} \right)^{k-1} \quad \frac{T_4}{T_3} = \left(\frac{P_4}{P_3} \right)^{\frac{k-1}{k}}$$

$$\eta_{th} = 1 - \frac{c_v(T_4 - T_1)}{c_v(T_3 - T_2)} = 1 - \frac{T_1}{T_2} = \boxed{1 - \frac{1}{r^{k-1}}}$$

Effect of Specific Heat Ratio

$$\eta_{th} = 1 - \frac{1}{r^{k-1}}$$

const c_v



Cylinder temperatures vary between 20K and 2000K where $1.2 < k < 1.4$