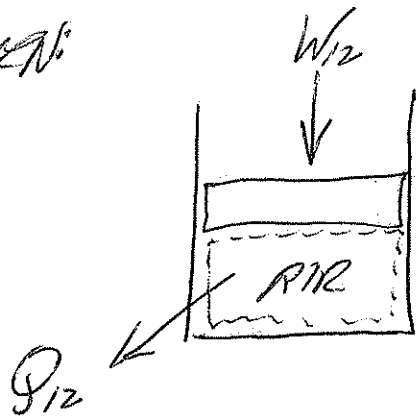


GIVEN:



IDEAL GAS

$$PV^n = \text{CONST} \rightarrow n = 1.25$$

$$m = .5 \text{ lbm}$$

$$T_1 = 500 \text{ R}$$

$$V_2 = 1 \text{ ft}^3$$

$$P_1 = 10 \text{ psia}$$

FINO: W_{12} , Q_{12}

SOLUTION:

P
(psia)

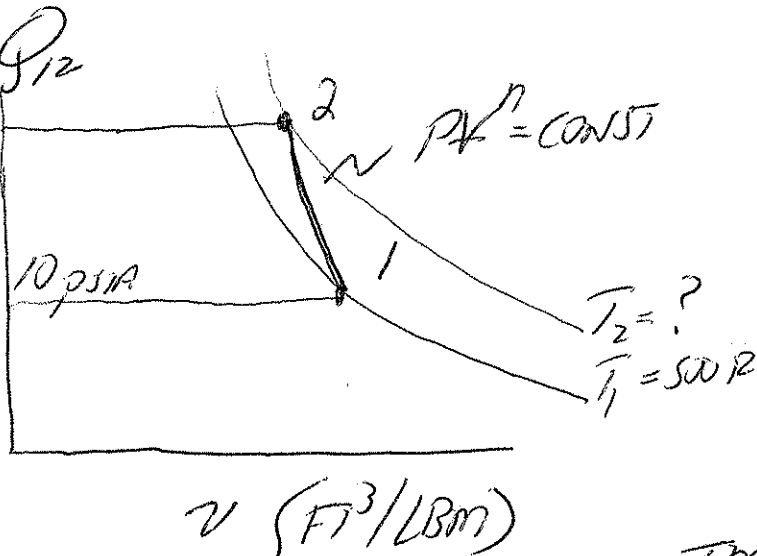


TABLE C.13a

STEEL

$$P_1 = 10 \text{ psia}$$

$$T_1 = 500 \text{ R}$$

$$v_1 = \frac{RT_1}{P_1} = \frac{\left(53.34 \frac{\text{ft} \cdot \text{lbf}}{\text{lbm} \cdot \text{R}}\right) (500 \text{ R})}{\left(10 \frac{\text{lbf}}{\text{in}^2}\right) \left(144 \frac{\text{in}^2}{\text{ft}^2}\right)}$$

$$v_1 = 18.52 \text{ ft}^3/\text{lbm}$$

$$u_1 = 85.2 \text{ Btu/lbm}$$

$$h_1 = 119.48 \text{ Btu/lbm}$$

TABLE C.16a

STEEL

$$v_2 = v_2 / \rho_m = 157^3 / .5 / \text{lbm} = 2.57^3 / \text{lbm}$$

$$P_2 = P_1 (v_2 / v_1)^n = 10 \text{ psia} \left(\frac{2.57^3 / \text{lbm}}{18.5257^3 / \text{lbm}} \right)^{1.25}$$

$$P_2 = 161.53 \text{ psia}$$

$$T_2 = T_1 (v_2 / v_1)^{1-n} = (500 \text{ R}) \left(\frac{2.57^3 / \text{lbm}}{18.5257^3 / \text{lbm}} \right)^{1-1.25}$$

$$T_2 = 872 \text{ R}$$

$$\left. \begin{array}{l} u_2 = 149.7 \text{ Btu/lbm} \\ h_2 = 209.4 \text{ Btu/lbm} \end{array} \right\} \begin{array}{l} \text{INTERPOLATING} \\ \text{FROM TABLE C.16a} \end{array}$$

RESPONDING 1st LAW

$$Q_{12} - W_{12} = m(u_2 - u_1) + \Delta KE + \Delta PE$$

FOR POLYTROPIC PROCESS, $n \neq 1$

$$W_{12} = (P_2 v_2 - P_1 v_1) / 1-n = \frac{mR(T_2 - T_1)}{1-n}$$

$$W_{12} = \frac{(.5 / \text{lbm}) (.287 \frac{\text{Btu}}{\text{lbm} \cdot \text{R}}) (872.2 - 500) \text{ R}}{1 - 1.25} = \underline{\underline{-51 \text{ Btu}}}$$

$$Q_{12} = m (U_2 - U_1) + W_{12}$$

$$Q_{12} = (.5 \text{ lbm}) (149.65 - 85.2) \frac{\text{Btu}}{\text{lbm}} + -51 \text{ Btu}$$

$$Q_{12} = \underline{\underline{-18.8 \text{ Btu}}}$$

Reflection:

COMPRESSION PROCESS \rightarrow WORK DONE \rightarrow -VE

POLYTROPES ARE BETTER THAN ISOTHERMS!

RMC TABLES AVOID MESSY INTERPOLATION OF C_v, C_p !

$$\Delta U = \int_1^2 C_v(T) dT \quad \Delta h = \int_1^2 C_p(T) dT$$